

# FLEXIBLE TRAJECTORY GENERATION TO EXTEND HUMAN-ROBOT INTERACTION WITH DYNAMIC ENVIRONMENT ADAPTATION

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Abstract: In our daily life, we use many elements that help us by means of a higher protection level (thimble, door stop) or by improving our dexterity (funnel, compasses). Both kinds of elements allow us to execute well known tasks with less concentration, faster, and, above all, improving performance. Like the real tools mentioned above, in the robotics field, virtual constraints enhance human-machine interaction. This work presents a multi-parametric behaviour model for an agent that increases task safety, and enables higher integration possibilities. The model presented here allows the perturbation of a programmed task, by introducing virtual elastic and viscous forces. This work presents the behaviour model, a description of it's implementation and experimental results in human-robot interaction.

## 1 INTRODUCTION

Some robotic applications need to benefit from the accuracy and precision of a robotic system, while preserving a degree of human control. Some of such application fields are assistive or surgical robotics. The goal of a robotic assistant is to provide motion commands that enhance precision, stability, safety and skilfulness. Significant research of assistant robotics systems is illustrated in Dario et al (1999), as an assistant for colonoscopy. In assistive robotics, due to the difficulties in modelling the environment with enough definition or under changing scenarios, it is necessary to aid the robotic arm to adapt its movements to the real environment or to the needs of the user.

These requirements have motivated the study and development of behaviour models. The model must allow software-generated force, velocity and position signals applied to human operators through the robotic system. A behaviour model can improve human performance in robot-assisted manipulation tasks, restricting movements into a region, constraining velocities in a specific direction and/or

introducing virtual correction forces. The presented multi-parametric behaviour model allows perturbing on-line a predefined path, applying forbidden region restrictions, and tuning model parameters (like masses, viscosity, and stiffness).

There's many procedures performed nowadays by surgical robots, most of them are in the orthopaedic field, using CAD/CAM surgical systems, or teleoperated surgical robots for laparoscopic interventions. Examples of successful procedures performed with the Zeus system are reported in Zhou et al (2006). This success has been achieved as a result of the human enhancement that robotic-assisted surgery systems offer.

Despite this success, there are several key challenges that require to be solved in order to achieve a complete development of surgical robotic systems. Kanade (2004) carries out an analysis of technological barriers. Introduced in Rosenberg (1993), virtual fixtures are playing an important role in the development of human-machine cooperative interaction enhancement. Several groups have integrated different implementations of virtual fixtures in surgical robotic systems, as described in

Bettini et al (2002). The work presented increases human capabilities, integrating three categories of restrictions: geometric, kinematic and dynamic. On the other hand, by being a parametric representation, different responses can be achieved with the same model. Changing the virtual mass, length, elasticity and viscosity... the behaviour can be tuned according to specifications of a certain task.

## 2 FLEXIBLE TRAJECTORY GENERATION

### 2.1 Task Oriented Trajectories

Many robots execute tasks by repeating a programmed sequence of movements. These sequences can be stored either with teaching by demonstration techniques or by using the corresponding robot programming language.

The work presented here aims to provide some means of changing this trajectory during the execution of the programmed task, through the action of a human that perturbs the robot movement by steering the end effector in the desired direction, with a given force,  $F$ .

The developed method is based on the definition of the robot path by means of two functions:  $A(t) = (x, y, z)$  and  $B(t) = (x, y, z)$ . As the Figure 1 shows, the segment defined by  $P_1$  and  $P_2$  is considered the non-perturbed position of the end-effector.

The programmed path can be modified if an external force is applied on the robot, or the presence of an obstacle is detected on its way. In both cases, the trajectory is modified producing an elastic movement away from the trajectory of the end-effector. Considering the two trajectory functions  $A(t)$  and  $B(t)$ , the resulting behaviour can be compared with a cable car, where the cabin is modelled by a linear segment held from two extreme points. The two links are springs with non linear behaviour endowed with damping. In this way the end-effector trajectory (the cabin) can be moved away with respect to the theoretical trajectory (the cable) by applying a perturbation force which is perceived by the user itself.

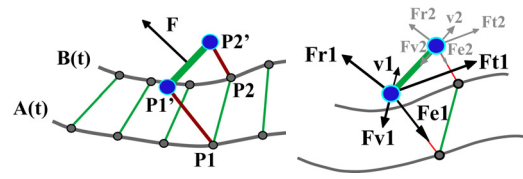


Figure 1: End-effector trajectory and the resulting forces.

The perturbation of the position caused by an external interaction produces a movement away from the position of the segment  $P_1(t) - P_2(t)$ . The representation for one such segment can be seen in Figure 1.

The perception of the increasing effort enables us to get better results to produce smooth movements with a reasonable effort of the user. The distance  $P_1 - P_1'$  and  $P_2 - P_2'$  that can be produced in each movement is the result of the following four set of forces: Two vectors  $Fr_1$  and  $Fr_2$  equivalent to the forces and torques measured on the force sensor. A second component is an elasticity force  $Fe_1$  and  $Fe_2$ . A third element is an attraction force  $Ft_1$  and  $Ft_2$ , towards the non perturbed trajectory. And a fourth factor corresponds to viscosity,  $Fv$ , that contributes to smoothing the trajectory when the robot returns to its programmed trajectory after a perturbation.

The forces that appear at each instant are shown in Figure 1. The resultant of these two systems, of four forces each, is what determines the segment dynamics.

### 2.2 Behaviour Model for the Human-Robot Interaction

The implementation of this model uses the motion equation for a rigid body. Below, the structure of this implementation is described, as well as several equations and concepts needed. For a system of  $n$  particles  $X(t)$  extends to

$$X(t) = (x(t) \quad v(t))^T \tag{1}$$

We define the sum of forces acting at this particle at time  $t$  as  $F(t)$ . Then, if the particle's mass is  $m$ , the change of  $X(t)$  is defined by

$$\frac{d}{dt} X(t) = (v(t) \quad F(t)/m)^T \tag{2}$$

Given these equations, a simulation starts with initial conditions for  $X(0)$  and uses a numerical

solver to trail the change of  $X$  over time. When simulating a rigid body,

$$X(t) = (x(t) \ R(t) \ P(t) \ L(t))^T \quad (3)$$

With  $R(t)$  representing the orientation of the body,  $P(t) = M \cdot v(t)$  it's linear momentum and  $L(t) = I(t) \cdot \omega(t)$  it's angular momentum. Where the mass,  $M$ , of the solid is constant; and the inertia tensor is computed as  $I(t) = R(t)I_{body}R(t)^T$ , with  $I_{body}$  also constant. With this, (2) is now

$$\frac{d}{dt} X(t) = (v(t) \ \omega(t) * R(t) \ F(t) \ \tau(t))^T \quad (4)$$

Where  $F(t)$  is the sum of forces applied to the body, and  $\tau(t)$  is the sum of torques applied to it.

Arrived at this point, different behaviours can be designed and implemented changing parameters like the mass, and the inertia tensor. But what brings further capabilities of this model is the insertion of virtual forces and torques, so that  $F(t)$  and  $\tau(t)$  become the sum of the external actions and the virtual ones. This virtual forces and torques are designed to add different types of constraints like impedance walls, viscosity of the medium, forbidden regions or elastic correction forces.

The basis of the proposed model is defined as a rigid body with two masses and a rigid link between them. The virtual environment is a spring connection element between each of the masses and a reference point, as well as a viscosity of the medium.

Using this model, the reference point location, damping, elasticity, mass and rigid link length are parameters. Also, a constant virtual force can be added to the system in either solid or world reference. The equations of the virtual forces in the solid reference frame are:

$$A1_{solid} = R(t)^{-1} * (A1_{world} - x(t)_{world}) \quad (5)$$

$$F1_{viscous}(t) = (v(t)_{solid} + \omega_{solid} \times P1_{solid}) \cdot (-c) \quad (6)$$

$$F1_{elastic}(t) = (A1_{solid}(t) - P1_{solid}) \cdot (k) \quad (7)$$

$$F1_{solid}(t) = F1_{elastic}(t) + F1_{viscous}(t) + F1_{constant}(t) \quad (8)$$

$$\Gamma1_{solid}(t) = P1_{solid} \times F1_{solid}(t) + \Gamma1_{constant}(t) \quad (9)$$

The analogous equations can be written for the second mass. At this point, the external forces can be included in the model, and the resulting forces and torques in the world reference are

$$F1_{world}(t) = R(t) * (F1_{solid}(t) + F2_{solid}(t) + F_{extern}(t)) \quad (10)$$

$$\Gamma1_{world}(t) = R(t) * (\Gamma1_{solid}(t) + \Gamma2_{solid}(t) + \Gamma_{extern}(t)) \quad (11)$$

The added value that this model of behaviour provides is based on the fact that both virtual and

real interactions are defined with a natural, intuitive and transparent approach.

From the dynamic behaviour point of view, the parameters that have been tuned for a desired response are the mass, distance between the spheres, viscosity of the medium and elasticity of the virtual links.

These parameters can be fixed for a desired performance during the execution of a task, but their values can also be tight to a parameter that evolves during the execution of the task. This dynamic adaptation can be model based and environment based. In the first case, both viscosity and elasticity parameters are function of the minimum distance to an object.

### 3 EXPERIMENTAL SYSTEM

An experimental setup has been designed in order to evaluate the different behaviours, shown in Figure 2. The system developed includes a 6 degrees of freedom robotic arm manufactured by Stäubli, a motion controller by Adept, an ATI force and torque sensor and a Dell personal computer.

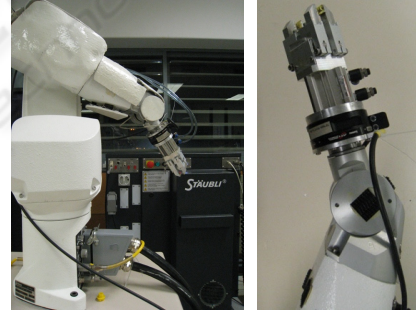


Figure 2: Experimental system used for the evaluation of the proposed behaviour.

The robotic arm is initially programmed to perform task. The trajectory is specified by either position and orientation, transformation matrices or two trajectory paths as mentioned before. Geometric, cinematic and dynamic restrictions of the robotic arm are also considered when the trajectory is programmed.

The motion controller is programmed with a low level firmware that computes motion commands. A hybrid position/force control loop is running with a 16 millisecond period time. Motion orders can be sent in either Cartesian or Joint type, as well as in either incremental or absolute modes. The motion

controller runs a communication server under TCP/IP protocol.

The force sensor measures forces and torques applied at the tool sustained by the robot. An analog to digital converter hardware and a calibration routine are called by the personal computer. As a result, two vectors are ready to be introduced to the behaviour model: external forces and torques.

The personal computer runs the hybrid force/position control loop linked to the motion controller and the force/torque sensor. As described in next section, a set of algorithms have been developed to accomplish all computing requirements.

The control loop accomplishes the main functionality of the software developed for the system. The sequence of routines called at each cycle is:

- Capture position and orientation of the robot
- Capture voltages at the force sensor
- Compute forces and torques from voltages
- Subtract weight of the tool using its orientation
- Calculate new state according to the behaviour
- Send new state to the motion controller

## 4 RESULTS AND CONCLUSIONS

The model proposed, based on a double virtual mass body, and elastic and viscous links has been tested with some results shown in Figure 3. Different experiments have been designed and tested. Simple tasks like object pick and place, path following or surface polishing are accomplished. During the execution of the overall task, a perturbation is introduced by means of external forces and torques. The system reacts to the perturbations measured by the force sensor, computing new positions according to the described model, and sending the perturbed positions to the motion controller. After the real perturbation, the virtual forces described earlier act as guidance of the endpoint, smoothly driving the end effector back to the pre-programmed path.

In order to increase human capabilities, some cooperative tasks include virtual constraints. The proposed model integrates three categories of restrictions: geometric, kinematic and dynamic. In order to accomplish the geometric constraints, a proximity library (Giralt and Hernansanz 2006) and a surface navigation method (Hernansanz et al 2007) have been developed and incorporated.

As it's a parametric model, different responses can be achieved with the same model. By changing the values of the virtual mass, elasticity and

viscosity, the behaviour can be tuned according to specifications of a certain task.

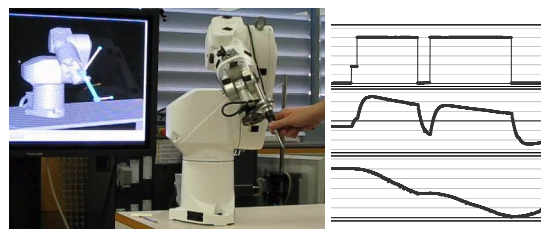


Figure 3: Experimental results. The left picture shows the perturbation of a trajectory by means of external forces. The two below the picture describe numerical values of the reaction. First graph is the evolution of the external force applied to the endpoint of the manipulator. The graph in the middle shows the evolution of velocity of the end effector. Last graph describes position response to these force steps.

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