

Fast Assessment of Wildfire Spatial Hazard with GPGPU

Donato D'Ambrosio¹, Salvatore Di Gregorio¹, Giuseppe Filippone¹, Rocco Rongo²,
William Spataro¹ and Giuseppe A. Trunfio³

¹Department of Mathematics, University of Calabria, 87036 Rende, CS, Italy

²Department of Earth Sciences, University of Calabria, 87036 Rende, CS, Italy

³Department of Architecture, Planning and Design, University of Sassari, 07041 Alghero, SS, Italy

Keywords: GPGPU, Cellular Automata, Wildfire Simulation, Wildfire Susceptibility, Hazard Maps.

Abstract: In the field of wildfire risk management the so-called *burn probability maps* (BPMs) are increasingly used with the aim of estimating the probability of each point of a landscape to be burned under certain environmental conditions. Such BPMs are computed through the explicit simulation of thousands of fires using fast and accurate simulation models. However, even adopting the most optimized simulation algorithms, the building of simulation-based BPMs for large areas results in a highly intensive computational process that makes mandatory the use of high performance computing. In this paper, General-Purpose Computation with Graphics Processing Units (GPGPU) is applied, in conjunction with a specifically devised wildfire simulation model, to the process of BPM building. Using two different GPGPU devices, the paper illustrates two different implementation strategies and discusses some numerical results obtained on a real landscape.

1 INTRODUCTION

Systematic risk-assessment procedures are increasingly considered as important components of the multifaceted strategy for mitigating the harmful impact of wildfires. Among the different tools to support fire hazard management, there are the so-called *burn probability maps* (BPMs), which attempt to provide an estimate of the probability of a point in a landscape to be burned under certain environmental conditions. Since the many factors that determine the fire behaviour interact nonlinearly to determine the hazard level, models for simulating wildfire spread are increasingly being used to build BPMs (Carmel et al., 2009; Ager and Finney, 2009). In particular, the typical approach is based on carrying out a high number of simulations (e.g. many thousands), under different weather scenarios and ignition locations (Carmel et al., 2009).

In order to obtain reliable results in reasonable time, such an approach must be based on fast and accurate simulation models operating on high-quality high-resolution remote sensing data (e.g., Digital Elevation Models, vegetation description, etc.). Among the different wildfire simulation techniques (Sullivan, 2009), those based on Cellular Automata (CA) (Kourtz and O'Regan, 1971; Lopes et al., 2002; Trun-

fio, 2004; Yassemi et al., 2008; Peterson et al., 2009) represent an ideal approach to build a BPM. This is because they provide accurate results and can often perform the same simulations in a fraction of the run time taken by different methods (Peterson et al., 2009).

However, because of the required high number of explicit fire propagations, even using the most optimized algorithm, the building of simulation-based BPMs often results in a highly intensive computational process. This is particularly true when the BPM concerns a large area. For example, building a high-resolution BPM covering a regional territory can be often infeasible using standard computing facilities.

In the latest years, while the computational needs of such sophisticated risk-assessment procedures have been increasing, the same happened to the availability of high-performance computers. A variety of parallel computing systems are available today, including massive parallel computers, clusters, computational grids, multi-core CPU computers and the recently emerging General-Purpose computing on Graphics Processing Units (GPGPU), in which multi-core Graphics Processing Units (GPU) perform computations traditionally carried out by the CPU.

In this paper, GPGPU is applied, in conjunction with a wildfire simulation model, to the process of

BPM computation. In particular, the proposed approach is based on a CA simulation approach which represents a suitable tradeoff between accuracy and speed of execution. The adopted parallel computation consists of the iterative simultaneous simulation of a number of wildfires with GPGPU, in order to cover the whole area under study. The paper illustrates two different implementation strategies in terms of model parallelisation, which correspond to different performances in terms of computing time. In addition, using two different GPGPU devices some numerical results obtained on a real Mediterranean landscape, which is historically characterized by a high incidence of wildfires, are discussed.

The paper is organized as follows. The next section outlines the main characteristics of the adopted CA simulation model and illustrates some details of the typical approach for BPM computation. Then, in section 3 some introductory elements of the adopted GPGPU approach are presented. Section 4 outlines the proposed parallel approaches and in section 5 some of their computational characteristics are empirically investigated. The paper ends with section 6 in which we draw some conclusions and outline possible future work.

2 A CA FOR FAST WILDFIRE SIMULATION AND SPATIAL HAZARD ASSESSMENT

As most wildfire spread simulators, the approach adopted in this paper is based on the Rothermel fire model (Rothermel, 1972; Rothermel, 1983), which provides the heading rate and direction of spread given the local landscape and wind characteristics. An additional constituent is the commonly assumed elliptical description of the spread under homogeneous conditions (i.e. spatially and temporally constant fuels, wind and topography) (Alexander, 1985). Under the above hypothesis, given the assumption of homogeneity at the cell level, the CA transition function uses the elliptical model for producing the complex patterns that correspond to the fire spread in heterogeneous conditions.

As mentioned above, CA methods for simulating wildfire can be highly optimized from the computational point of view. For this reason they are well suited for the process of building BPMs. Nevertheless, a well-known problem associated with the cell-based methods is the distortion that may affect the produced fire shape. For example, as shown later in Section 2.1, under homogeneous conditions and in

presence of wind, the shape of the heading portion of the fire is often angular rather than rounded as in the expected ellipse (French et al., 1990). Unfortunately, such systematic errors under homogeneous conditions typically correspond to inaccurate results also in real applications (Cui and Perera, 2008; Peterson et al., 2009) and in thus in the computation of BPMs.

Several studies have recognized that the distorted shapes are caused by the fire only being able to propagate along the small number of fixed directions imposed by the raster (French et al., 1990; Johnston et al., 2008; Peterson et al., 2009).

The CA-based method adopted in this paper provides a satisfactory level of accuracy thanks to some of the ideas already presented in the literature, namely extending the size of the neighbourhood (O'Regan et al., 1976; French et al., 1990) and avoiding centre-to-centre ignitions between cells (Johnston et al., 2008; Trunfio et al., 2011). However, instead of using a random irregular grid as in (Johnston et al., 2008), here the randomization is explicitly introduced over the regular lattice according to the approach proposed by (Miyamoto and Sasaki, 1997) for simulating lava flows through CA. Moreover, the run time efficiency of the model is significantly high thanks to an adaptive time step strategy (Peterson et al., 2009), which simulates the progression of the fire by avoiding unnecessary computation.

2.1 Model Description

As in different CA-based wildfire simulation models (Trunfio, 2004; Peterson et al., 2009), the two-dimensional fire propagation is simulated through a growing ellipse having the semi-major axis along the direction of maximum spread, the eccentricity related to the intensity of the so-called *effective wind* and one focus acting as a 'fire source'.

At each time step the ellipse's size is incremented according to both the duration of the time step and maximum rate of spread (see Figure 1). Afterwards, a neighbouring cell invaded by the growing ellipse is considered a candidate to be ignited by the spreading fire. In case of ignition, a new ellipse is generated according to the amount of overlapping between the invading ellipse and the ignited cell.

More formally, the model is a two-dimensional CA with square cells defined as:

$$CA = \langle \mathcal{X}, \mathcal{N}, \mathcal{S}, \mathcal{P}, \omega, \Psi \rangle \quad (1)$$

where:

- \mathcal{X} is the set of points in the finite region where the phenomenon evolves. Each point represents the centre of a square cell;

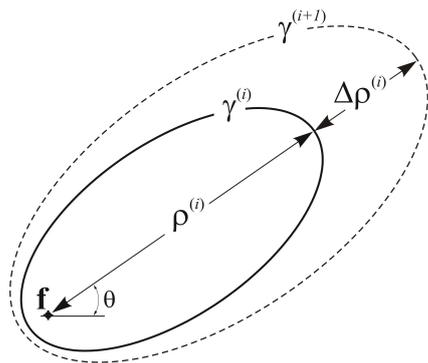


Figure 1: Growth of the ellipse γ locally representing the fire front. The symbol ρ denotes the forward spread which is incremented by $\Delta\rho$ at the i -th time step.

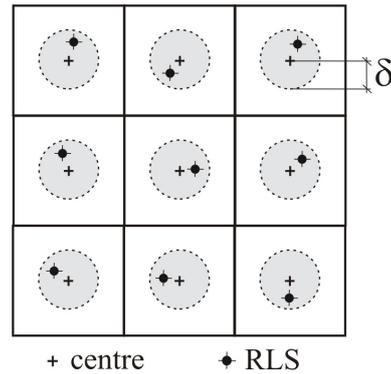


Figure 2: An example of RLSs arrangement in a subset of the automaton. Each RLS occupies a random position within a distance δ from the cell centre.

- Q is a set of *random local sources* (RLSs), one point for each cell; they are randomly generated at the beginning of the simulation within an assigned radius δ from each of the centres in \mathcal{K} , as shown in Figure 2. As detailed later, a new ignition in a cell consists of a new ellipse having its rear focus on the local source $\mathbf{q} \in Q$;
- \mathcal{N} is the set that identifies the pattern of cells influencing the cell state change (i.e the neighbourhood);
- \mathcal{S} is the finite set of the states of the cell, defined as the Cartesian product of the sets of definition of all the cell's substates;
- \mathcal{P} is the finite set of global parameters which define the fuel bed characteristics according to the standard fuel models used in BEHAVE (Andrews, 1986);
- $\omega: \mathcal{S}^{|\mathcal{N}|} \rightarrow \mathcal{S}$ is the transition function accounting for the fire ignition, spread and extinction mechanisms;
- Ψ is the set of global functions, activated at each step before the application of the transition function ω to modify either the values of model parameters in \mathcal{P} or the cells' substates. Among these, the function ϕ_τ adapts the size $p_{\Delta t}$ of the time step according to both the size of the cells p_e and current maximum spread rate in the whole automaton. The value of $p_{\Delta t}$ is then used by another function, ϕ_t , for keeping the current time up to date.

The cell's substates include all the local quantities used by the transition function for modelling the interactions between cells (i.e. fire propagation to neighbouring cells) as well as its internal dynamics (i.e. fire ignition and growth). In particular, the relevant components of the state of each cell are:

- the altitude $z \in \mathbb{R}$;

- the fuel model $\mu \in \mathbb{N}$, which is an index referring to one of the mentioned fuel models that specifies the characteristics of vegetation relevant to Rothermel's equations;
- the combustion state $\sigma \in \mathcal{S}_\sigma$, which takes one of the values *unburnable*, *not ignited*, *ignited* and *burnt*.
- the accumulated forward spread $\rho \in \mathbb{R}_{\geq 0}$, that is the current distance between the focus \mathbf{f} of the local ellipse and the farthest point on the semi-major axis (see Figure 1);
- the angle $\theta \in \mathbb{R}$ (see Figure 1), giving the direction of the maximum rate of spread. In the context of the semi-empirical Rothermel's approach, such an angle is obtained through the composition of two vectors, namely the so-called *wind effect* and *slope effect* (Rothermel, 1972), both obtained on the basis of the local wind vector, local terrain slope and fuel model;
- the maximum rate of spread $r \in \mathbb{R}_{\geq 0}$, also provided by Rothermel's equations on the basis of the relevant local characteristics (Rothermel, 1972);
- the eccentricity $\varepsilon \in [0, 1]$ of the ellipse γ representing the local fire front, which is obtained as a function of both the wind and terrain slope through the empirical relation proposed in (Anderson, 1983).

Among the remaining substates are the local wind vector and the relative humidity value of the cell, both provided as external input to the model.

As mentioned above, the CA model is based on an extended Moore's neighbourhood composed of 24 cells. Also, as explained below and represented in Figure 2, the use of RLSs inside each cell allows for obtaining a high number of different spread direction during the fire propagation in the landscape, thus significantly improving the accuracy of the results.

The transition function ω concerns only cells that are in the *burning* state. The first step of ω consists of checking the condition that triggers the transition to the *burnt* state. The latter is verified when all the neighbouring cells are in either the *ignited* or in the *unburnable* state, that is when the cell's contribution is no longer necessary to the fire spread mechanism.

Then, if the cell still belongs to the fire front, ω updates the size of the local ellipse γ . This is accomplished by adding to the accumulated forward spread ρ the product of the rate of spread r and the step size Δt . The latter is dynamically established by the global function ϕ_τ according to the procedure proposed by (Peterson et al., 2009).

The next step of ω consists of testing if the fire is spreading towards other cells c_i of the neighbourhood that are in the *not ignited* state. Since in the current cell the fire front is represented by a local ellipse γ , such a spread test is carried out through checking if γ includes the RLS q_i of the cell c_i (see Figure 3). To this purpose the current spread in direction q_i can be easily computed using the mathematical properties of the ellipse.

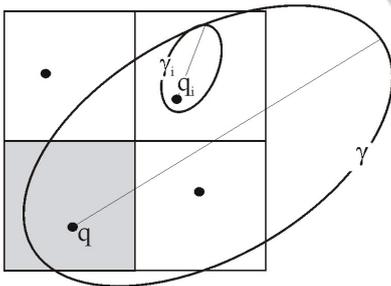


Figure 3: The i -th neighbouring cell intersected by the ellipse γ locally representing the fire front.

If q_i is inside γ , then a new ellipse γ_i is generated for the cell c_i , having the following characteristics:

- both the intensity r_i of the maximum spread rate vector and its inclination θ_i are computed through the proper Rothermel's equations (Rothermel, 1972);
- the eccentricity ε_i is determined using the empirical formula proposed by (Anderson, 1983), which accounts for both the effect of wind and topography through the previously mentioned *effective wind speed* (McAlpine et al., 1991).
- as shown in Figure 3, its size is initialized so that its most advanced point lies on the ellipse γ ;
- the RLS q_i is assumed as rear focus.

When compared with a typical CA algorithm for wildfire simulation, the main advantage of the ap-

proach based on the RLSs, lies in its ability to increase the directions of spread. This leads to an improved accuracy as shown in Figure 4, where the expected fire shape under homogeneous conditions is compared with the simulated shapes given by different CA approaches.

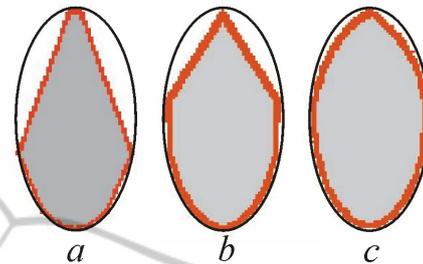


Figure 4: A comparison between the simulated fire shapes obtained under homogeneous condition with different CA approaches: a) standard CA based on the Moore's neighbourhood and on a centre-to-centre ignition scheme; b) CA based on an extended neighbourhood composed of 24 cells with a centre-to-centre ignition scheme; c) CA based on the same neighbourhood used in b) together with the RLSs. The continuous line represents the expected shape.

2.2 A Simulation-based Approach for Building BPMs

In the latest years, the use of hazard maps based on the explicit simulation of natural phenomena has been increasingly investigated as an effective and reliable tool for supporting risk management (Rongo et al., 2008; Carmel et al., 2009; Ager and Finney, 2009; Rongo et al., 2011).

In the case of wildfire, the most general approach for computing a BPM on a landscape (Carmel et al., 2009; Ager and Finney, 2009) consists of a Monte Carlo approach in which a high number of different fire spread simulations are carried out, sampling from suitable statistical distributions the random variables relevant to the fire behaviour. For example, the wind direction for each simulated fire can be sampled in a range corresponding to the typical directions of severe wind for the area. At the end of the process, the local risk is computed on the basis of the frequency of burning.

The technique for computing the BPMs adopted in this study is based on a prefixed number n of simulation runs, where each run represents a single simulated fire. The adopted weather scenario (i.e. wind and fuel moisture content) corresponds to extreme conditions for the area with regards to relevant historical fires. A regular grid of ignition locations is adopted, which corresponds to the assumption of a uniform ignition probability for each point of the

landscape. Also, all the simulated fires have the same duration. The latter is selected considering the duration of historical fires in the regions under study. All the other relevant characteristics are kept constant during the simulations.

Once the latter have been carried out, the resulting n maps of burned areas are overlaid and cells' fire frequency are used for the computation of the fire risk. In particular, a *burn probability* $p_b(\mathbf{c})$ for each cell \mathbf{c} is computed as:

$$p_b(\mathbf{c}) = \frac{f(\mathbf{c})}{n}; \quad (2)$$

where $f(\mathbf{c})$ is the number of times the cell \mathbf{c} is ignited during the n simulated fires. The burn probability for a given cell is an estimate of the likelihood that a cell will burn given a single random ignition within the study area and given the assumed conditions in terms of fire duration fuel moisture and weather.

According to the procedure described above, the number n of simulation runs depend on the resolution of the grid of ignition points. In general, it is not necessary to simulate a wildfire for each of the cells in the automaton. In fact, considering the usual resolution of landscape data, ignitions on adjacent cells produce very similar fire shapes. Nevertheless, as shown in the application example discussed later, the number of fire simulation needed for achieving a good BPM accuracy can be considerably high in case of study areas with great extensions.

3 PARALLEL COMPUTING WITH GPGPU

A natural approach to deal with the high computational effort related to construction of the BPMs, is the use of parallel computing. Among the different parallel architectures and computational paradigms, in the last years GPGPU has attracted the interest of many researchers (Preis, 2011; Roberts et al., 2010; Szerwinski and Güneysu, 2008; Filippone et al., 2011; Pallipuram et al., 2011; Krger et al., 2010). This is mainly due to the following reasons:

- the computational power of devices enabling GPGPU has exceeded that of standard CPUs by more than one order of magnitude;
- the price of a typical device for GPGPU is comparable to the price of a standard CPU;
- there has been a rapid increase in the programmability of these devices, which has facilitated the porting of many scientific applications leading to relevant parallel speedups (Krger et al., 2010).

Modern GPUs are multiprocessors with a highly efficient hardware-coded multi-threading support. The key capability of a GPU unit is thus to execute thousands of threads running the same function concurrently on different data (Single Instruction Multiple Data architecture). Hence, the computational power provided by such an architecture, which can easily reach a teraFLOP, can be fully exploited through a fine grained data-parallel approach when the same computation can be independently carried out on different elements of a dataset.

The particular GPGPU platform investigated in this paper is the one provided by nVidia, which consist of a group of Streaming Multiprocessors (SMs) in a single device. Each SM can support a limited number of co-resident concurrent threads, which share the SM's limited memory resources. Furthermore, each SM consists of multiple Scalar Processor (SP) cores.

In order to program the GPU, in this paper we use the C-language Compute Unified Device Architecture (CUDA), a programming model introduced in 2006 by nVidia Corporation for their GPUs (NVidia corp., 2010). In a typical CUDA program, sequential host instructions are combined with parallel GPGPU code. The idea underlying this approach is that the CPU organizes the computation (e.g. in terms of data pre-processing), sends the data from the computer main memory to the GPU global memory and invokes the parallel computation on the GPU device. After, and/or during the computation, the computed results are copied into the main memory for post-processing and output purposes. In some cases, the computing scheme outlined above can be enhanced including overlapping the CPU and GPU computation as well as overlapping memory copying with computation (NVidia corp., 2010; NVidia corp., 2012).

In CUDA, the GPGPU activation is obtained by writing device functions in C language, which are called *kernels*. When a kernel is invoked by the CPU, a number of threads (e.g. typically several thousands) execute the kernel code in parallel on different data. From the kernel code it is possible to distinguish the currently associated thread through some built-in variables (i.e. *threadIdx*, *blockIdx*, and *blockDim*). This allows to select from the device memory the data to associate to that particular thread (e.g. the cell of a CA). According to the nVidia approach to GPGPU, threads are grouped into blocks and executed on a SMs.

From a programmer's point of view, it is of a certain relevance to know that the GPU can access different types of memory. For example, a certain amount of fast shared memory (which can be used for some limited intra-block communication between threads)

can be assigned to each thread block. Also, all threads can access a slower but larger global memory which is on the device board but outside the computing chip. The device global memory is slower if compared with the shared memory, but it can deliver significantly (e.g. one order of magnitude) higher memory bandwidth than traditional host memory (i.e. the main computer memory). The latter is typically linked to the GPU card through a relatively slow bus. For example, in most hardware configurations accessing the host memory from the GPU can be more than 20 times slower in terms of bandwidth (i.e. Gb/s) than accessing the global memory. As a result, the parallel computation should be organised in such a way to minimize data transfers between the host and the device. For example, in some cases it is preferable to execute on the device code which is inefficient (e.g. because that specific part of the whole computation does not fit well with the GPGPU model of parallelism) instead of running it on the CPU, if this allows to avoid large amount of CPU-GPU data transfers.

4 GPGPU-BASED WILDFIRE RISK ASSESSMENT

The CA approach is known as one of the most typical parallel computation paradigm. In fact, the whole system is composed of a set of independent cells, which are influenced only by their neighbours. This allows for: (i) computing the next state of all the cells in parallel; (ii) accessing only the current neighbours' states during each cell's update, thereby giving the chance to increase the overall efficiency and making easier even the implementation on distributed memory machines. As in the sequential case, the typical CA parallel implementation involves two memory regions representing the *current* and *next* states for the cell. For each CA step, the neighbouring values from *current* are read by the transition function, which performs its computation and writes the new state value into the appropriate element of *next*.

In particular, the GPGPU parallel implementation of the CA illustrated above, accordingly to the recent literature in the field (Preis, 2011; Roberts et al., 2010; Szerwinski and Güneysu, 2008; Filippone et al., 2011), was based on the following design choices:

- one or more CUDA computational kernels (i.e. threads) are assigned to each cell of the automaton as in (Filippone et al., 2011);
- most of the automaton data (i.e. both the current and next memory areas mentioned above)

is stored in the GPU global memory. This involves: (i) initialising the current state through a CPU-GPU memory copy operation (i.e. from host to device global memory) before the beginning of the simulation and (ii) retrieving the final state of the automaton at the end of the simulation through a GPU-CPU copy operation (i.e. from device global memory to host memory). Also, at the end of each CA step a device-to-device memory copy operation is used to re-initialise the *current* values with the *next* values.

In order to speed up the access to memory, the automaton data in device global memory should be organised in a way to allow coalescing access. To this purpose, a best practice recommended by nVidia is to use of *structures of arrays* rather than *arrays of structures* in organising the memory storage of cell's properties (NVidia corp., 2012). Thus, while the typical sequential implementation of the CA model described in section 2 is based on structures or objects encapsulating all the cells substates, in the GPGPU implementation it was more convenient to use simple arrays to store the automaton. In particular, an array with the size corresponding to the total number of cells was allocated in the CPU memory for each of the CA substates. All of such arrays were then mirrored in the GPU together with some additional auxiliary arrays (e.g. for storing the neighbourhood structure and the model parameters).

A key step in the parallelisation of a sequential code for the GPU architecture according to the CUDA approach, consists of identifying all the sets of instructions that can be executed independently of each other on different elements of a dataset (e.g., on the different cells of the automaton). As mentioned in Section 3, such sequences of instructions are grouped in CUDA kernels, each transparently executed in parallel by the GPU threads. In particular, in the CA model for wildfire simulation outlined in section 2, two CUDA kernels have been developed:

- the kernel implementing the fire propagation mechanism (i.e. the CA transition function ω);
- the kernel for dynamically adapting the time-step duration. Since this involves finding the minimum of all allowed time-step sizes among the cells on the current fire front, such kernel simply implements a standard parallel reduction algorithm.

One of the critical aspects of the GPGPU implementation is related to the fact that in the whole automaton only the cells on the current fire front do actual computation in the transition function. Hence, launching one thread for each of the automaton cells results in a certain amount of dissipation of the GPU

computational power. For this reason, besides the standard CA implementation (SCA) in which the above mentioned kernels are applied to each cells of the automaton, a more optimized CA (OCA) has also been developed. In the OCA, the kernel that adapts the time-step size at each iteration, also computes the smallest rectangular bounding box (RBB) that includes any cells on the current fire front, as shown in Figure 5. Thus, the kernels implementing the CA step are mapped only on such RBB, in this way reducing the number of kernel launches and improving significantly the computational performance of the algorithm. It is worth noting that the same strategy has been developed for the sequential version of the program in order to obtain a fair comparison.

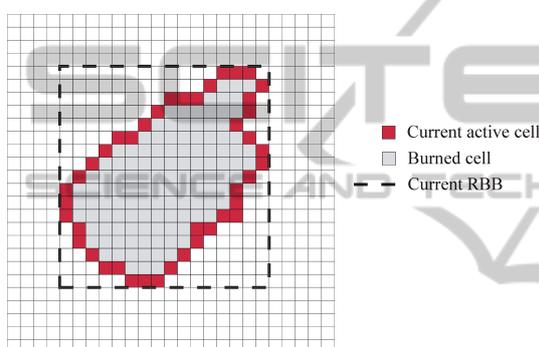


Figure 5: An example of the RBB representing the envelope of the current fire front. In the OCA version, the CUDA kernels are mapped only on the RBB.

However, notwithstanding the OCA approach, during the simulation of a single fire the RBB still includes a number of inactive cells. For example, all the burned cells inside the current fire front are typically included in the RBB though they are not computationally active. For this reason, in both the SCA and OCA version of the algorithm, more than a single fire are simultaneously simulated. In other words, the above mentioned kernels iterate over a number of active fires which are propagated simultaneously. Obviously, such an approach requires the use of an independent array for storing the combustion state σ of each cell of the automaton and for each simultaneous fire. At the cost of this additional memory occupation, the approach allows for increasing the level of device saturation with beneficial effects on the computing time.

Before starting the BPM construction, a pre-processing sequential phase takes place in which for each cell c_i the maximum rate of spread r_i , its direction θ_i and the local ellipse eccentricity ϵ_i (see Figure 1) are computed using the proper model equations (Rothermel, 1972; Anderson, 1983). According to the

algorithm outlined in section 2, such pre-computed quantities determine, together with the landscape topography, the wildfire spread at the cell-level. Also, during the pre-processing phase the maximum time-step size for each cell is computed and stored in an array in order to speed-up the time-step adaptation during the CA iterations.

The process for the BPM computation is organized as follows. Cluster of fires are iteratively simulated, up to covering the entire area under study (i.e. up to the required number n of fires). In order to maximize the advantages of the OCA approach described above, each cluster is composed of a block of contiguous fires taken from the regular grid of fire ignitions. For each cluster of simultaneous fires, the CA steps are iterated until the current time p_t reaches the final time. In the parallel implementation, each CA step essentially consists of the two CUDA kernels mentioned above plus the device-to-device memory copy operation to re-initialise the *current* values of the substates with the *next* values.

At the end of each group of simulations, a further CUDA kernel is launched on the whole automaton to update an array f_n in which each element represents the number of times that a cell has been burned since the beginning of the process. As soon as all the scheduled simulations have been carried out, each element of the array f_n , divided by the total number of simulations, gives an estimate of the burn probability for one of the cells.

5 RESULTS ON A REAL LANDSCAPE

The preliminary application presented here concerns an area of the Liguria region, in Italy, historically characterized by a high frequency of serious wildfires. The landscape, shown in Figure 6 was modelled through a Digital Elevation Model composed of 461×445 square cells with side of $40m$. In the area, the terrain is relatively complex with an altitude above sea level ranging from 0 to 250 m. The heterogeneous fuel bed depicted in Figure 6, was based on the use of the 1:25000 land cover map from the CORINE EU-project. The CORINE land-cover codes were mapped on the standard fuel models used by the CA (i.e., the substate μ). Plausible values of fuel moisture content were obtained from literature data. Also, a domain-averaged open-wind vector from the North direction, having an intensity of $20 km h^{-1}$, was used for producing time-constant gridded winds through WindNinja (Forthofer et al., 2009), a computer program that simulates the effect of terrain on the wind flow. A du-

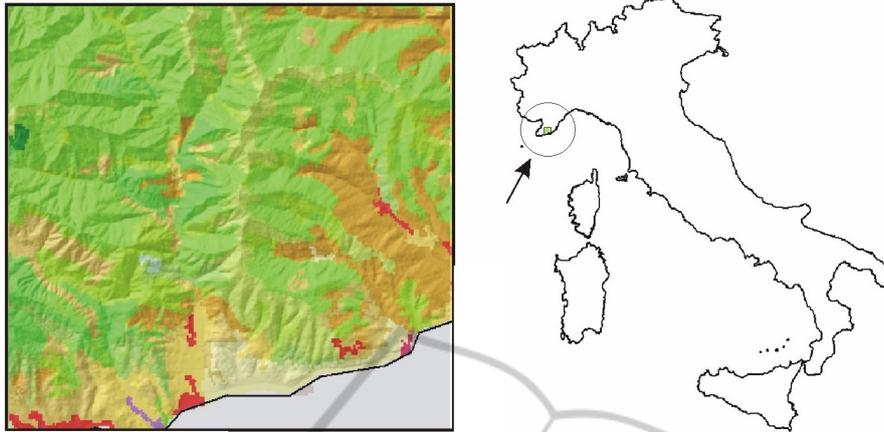


Figure 6: The landscape under study: a $18\text{km} \times 18\text{km}$ area in Liguria, Italy. Colors refer to the standard CORINE land-cover data.

ration of 10 hours was adopted for all simulated fires. Over the area, a regular grid of 91×88 ignition points was superimposed, leading to 8008 fires to simulate.

Two CUDA graphic devices were used in the experiments: a nVidia high-end Tesla C1060 and a nVidia Geforce GT430 graphic card. In Table 1 some of the relevant characteristics of the used GPGPU devices are reported. The sequential programs, implementing the same algorithms parallelised for the GPGPU version, were run on a desktop computer equipped with a 2.66 Ghz Intel Core 2 Quad CPU. The two different implementations SCA and OCA described in Section 4 were run on both the CPU and GPU devices. In both cases, during the computation process, 196 wildfires at a time were activated in order to attain a satisfactory level of saturation of the graphic device (see section 4).

The hazard map obtained after the $n = 8008$ simulations is shown in Figure 7. As shown in Table 2, using the CPU the task took about $2.37h$ for the SCA version and about $1.44h$ for the OCA implementation. As it can be seen in the same Table 2, the gain provided by the parallelisation in terms of computing time is significant. In particular, through the most powerful GPGPU the BPM computation took only 5 minutes using the SCA implementation and about 3.5

Table 1: Characteristics of the adopted GPGPU hardware for all carried out experiments.

	GT430	Tesla C1060
Compute capability	2.1	1.3
CUDA cores	96	240
Global memory [MB]	1024	4096
Clock rate [MHz]	1400	1300
Bandwidth [GB/s]	28.8	102.4
GFLOPs	268.8	922.12

Table 2: Elapsed times (in seconds) for the computation of the BPM shown in Figure 7.

	SCA	OCA
CPU	8518.2	5185.6
GT430	771.6	417.5
Tesla C1060	301.7	209.1

Table 3: Parallel speedup achieved with the used GPGPU devices.

	SCA	OCA
GT430	11.0	12.4
Tesla C1060	28.2	24.8

minutes using the OCA. Interestingly, even by using the consumer-level GPGPU GT430, the computation took only a few minutes.

According to Table 3, where the results in terms of parallel speedups are shown, the highest speedup of 28.2 was achieved by the Tesla C1060 using the SCA approach. Overall, the results in terms of time savings are significant, also considering the relatively little effort required to develop the parallel versions of the BPM computation algorithms. As before, it is also worth noting that the GT430 graphic card, which provided here a parallel speedup of more than 10, costs less than 60 Euros at the time of this publication.

As GPUs are specialized for single-precision calculations, comparison tests were eventually carried out with the aim of verifying the precision of results between CPU-based outputs and GPUs' ones. Here, results were satisfactory, since the areal extensions of simulations resulted the same, except for few approximation errors, limited to the 4th significant digit place, in a limited number of cells.

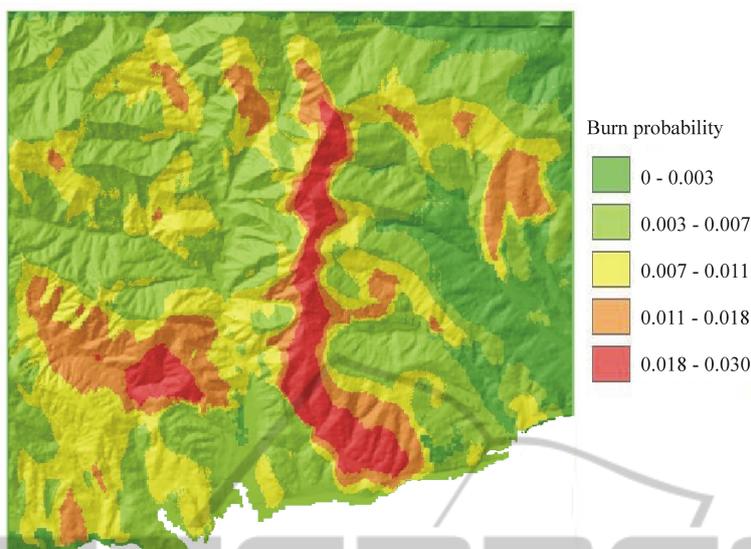


Figure 7: The BPM obtained for the landscape under study.

6 CONCLUSIONS AND FUTURE WORK

The results in terms of parallel speedup of the GPGPU-based BPM computation procedure presented above are indeed very encouraging. The main advantage of such a parallelisation lies in enabling the building of BPMs for large areas (e.g. at a regional level), which otherwise may not be possible by adopting standard architectures.

Nevertheless, since not all the available GPGPU optimization strategies have been implemented, ample margins of speedup improvement are still possible. For example, since the only active cells are the ones on the current fire front, even the OCA approach described above can permit to launch a significant number of kernels on cells which are inactive. A more advanced strategy could be used to map mono-dimensional execution blocks only on the minimal number of cells lying on the fire front. An empirical investigation will determine whether the complexity related to the building of such complex grid mapping would be compensated by the fewer kernels to launch at each step of the automaton.

Another possible direction of research consists of making available the GPGPU approach in more general libraries for supporting CA modelling and simulation, such as the one presented in (Blecic et al., 2009).

ACKNOWLEDGEMENTS

This work was partially funded by the European Commission - European Social Fund (ESF) and by the Regione Calabria (Italy).

REFERENCES

- Ager, A. and Finney, M. (2009). Application of wildfire simulation models for risk analysis. In *Geophysical Research Abstracts, Vol. 11, EGU2009-5489, EGU General Assembly*.
- Alexander, M. (1985). Estimating the length-to-breadth ratio of elliptical forest fire patterns. In *Proc. 8th Conf. Fire and Forest Meteorology*, pages 287–304.
- Anderson, H. (1983). Predicting wind-driven wildland fire size and shape. Technical Report INT-305, U.S Department of Agriculture, Forest Service.
- Andrews, P. (1986). BEHAVE: fire behavior prediction and fuel modeling system - burn subsystem, part 1. Technical Report INT-194, U.S Department of Agriculture, Forest Service.
- Blecic, I., Cecchini, A., and Trunfio, G. A. (2009). A general-purpose geosimulation infrastructure for spatial decision support. *Transactions on Computational Science*, 6:200–218.
- Carmel, Y., Paz, S., Jahashan, F., and Shoshany, M. (2009). Assessing fire risk using monte carlo simulations of fire spread. *Forest Ecology and Management*, 257(1):370 – 377.
- Cui, W. and Perera, A. H. (2008). A study of simulation errors caused by algorithms of forest fire growth models. Technical Report 167, Ontario Forest Research Institute.

- Filippone, G., Spataro, W., Spingola, G., D'Ambrosio, D., Rongo, R., Perna, G., and Di Gregorio, S. (2011). GPGPU programming and cellular automata: Implementation of the sciara lava flow simulation code. In *23rd European Modeling and simulation Symposium (EMSS)*, Rome, Italy.
- Forthofer, J., Shannon, K., and Butler, B. (2009). Simulating diurnally driven slope winds with windninja. In *Proceedings of 8th Symposium on Fire and Forest Meteorological Society - Kalispell, MT*.
- French, I., Anderson, D., and Catchpole, E. (1990). Graphical simulation of bushfire spread. *Mathematical Computer Modelling*, 13:67–71.
- Johnston, P., Kelso, J., and Milne, G. (2008). Efficient simulation of wildfire spread on an irregular grid. *International Journal of Wildland Fire*, 17:614–627.
- Kourtz, P. H. and O'Regan, W. G. (1971). A model for a small forest fire to simulate burned and burning areas for use in a detection model. *Forest Science*, 17(7):163–169.
- Krger, F., Maitre, O., Jimenez, S., Baumes, L., and Collet, P. (2010). Speedups between x70 and x120 for a generic local search (memetic) algorithm on a single gpgpu chip. In Di Chio, C., Cagnoni, S., Cotta, C., Ebner, M., Ekárt, A., Esparcia-Alcazar, A., Goh, C.-K., Merelo, J., Neri, F., Preu, M., Togelius, J., and Yannakakis, G., editors, *EvoNum 2010*, volume 6024 of *LNCS*, pages 501–511. Springer Berlin / Heidelberg.
- Lopes, A. M. G., Cruz, M. G., and Viegas, D. X. (2002). Firestation - an integrated software system for the numerical simulation of fire spread on complex topography. *Environmental Modelling and Software*, 17(3):269–285.
- McAlpine, R., Lawson, B., and Taylor, E. (1991). Fire spread across a slope. In *Proceedings of the 11th Conference on Fire and Forest Meteorology (Society of American Foresters: Bethesda, MD)*, pages 218–225.
- Miyamoto, H. and Sasaki, S. (1997). Simulating lava flows by an improved cellular automata method. *Computers & Geosciences*, 23(3):283–292.
- NVidia corp. (2010). CUDA C Programming Guide v. 3.2. NVidia corp. (2012). CUDA C Best Practices Guide.
- O'Regan, W. G., Kourtz, P., and Nozaki, S. (1976). Bias in the contagion analog to fire spread. *Forest Science*, 22.
- Pallipuram, V., Bhuiyan, M., and Smith, M. (2011). A comparative study of GPU programming models and architectures using neural networks. *The Journal of Supercomputing*, pages 1–46.
- Peterson, S. H., Morais, M. E., Carlson, J. M., Dennison, P. E., Roberts, D. A., Moritz, M. A., and Weise, D. R. (2009). Using HFIRE for spatial modeling of fire in shrublands. Technical Report PSW-RP-259, U.S. Department of Agriculture, Forest Service, Pacific Southwest Research Station, Albany, CA.
- Preis, T. (2011). GPU-computing in econophysics and statistical physics. *The European Physical Journal - Special Topics*, 194(1):87–119.
- Roberts, M., Sousa, M. C., and Mitchell, J. R. (2010). A work-efficient gpu algorithm for level set segmentation. In *ACM SIGGRAPH 2010 Posters*, SIGGRAPH '10, pages 53:1–53:1, New York, NY, USA. ACM.
- Rongo, R., Lupiano, V., Avolio, M. V., D'Ambrosio, D., Spataro, W., and Trunfio, G. A. (2011). Cellular automata simulation of lava flows - applications to civil defense and land use planning with a cellular automata based methodology. In Kacprzyk, J., Pina, N., and Filipe, J., editors, *SIMULTECH 2011*, pages 37–44. SciTePress.
- Rongo, R., Spataro, W., D'Ambrosio, D., Avolio, M. V., Trunfio, G. A., and Gregorio, S. D. (2008). Lava flow hazard evaluation through cellular automata and genetic algorithms: an application to mt etna volcano. *Fundam. Inform.*, 87(2):247–267.
- Rothermel, R. C. (1972). A mathematical model for predicting fire spread in wildland fuels. Technical Report INT-115, U.S. Department of Agriculture, Forest Service, Intermountain Forest and Range Experiment Station, Ogden, UT.
- Rothermel, R. C. (1983). How to predict the spread and intensity of forest and range fires. Technical Report INT-143, U.S. Department of Agriculture, Forest Service, Intermountain Forest and Range Experiment Station, Ogden, UT.
- Sullivan, A. (2009). Wildland surface fire spread modelling, 1990-2007. 3: Simulation and mathematical analogue models. *International Journal of Wildland Fire*, 18:387–403.
- Szerwinski, R. and Güneysu, T. (2008). Exploiting the power of GPUs for asymmetric cryptography. In *Proceedings of the 10th International Workshop on Cryptographic Hardware and Embedded Systems (CHES 2008)*, pages 79–99, Washington, DC, USA.
- Trunfio, G. A. (2004). Predicting wildfire spreading through a hexagonal cellular automata model. In Sloot, P. M. A., Chopard, B., and Hoekstra, A. G., editors, *ACRI*, volume 3305 of *LNCS*, pages 385–394. Springer.
- Trunfio, G. A., D'Ambrosio, D., Rongo, R., Spataro, W., and Gregorio, S. D. (2011). A new algorithm for simulating wildfire spread through cellular automata. *ACM Trans. Model. Comput. Simul.*, 22(1):6.
- Yassemi, S., Dragicevic, S., and Schmidt, M. (2008). Design and implementation of an integrated GIS-based cellular automata model to characterize forest fire behaviour. *Ecological Modelling*, 210(1-2):71–84.