# **Evaluation of Embedded Camera Systems for Autonomous Wheelchairs**

Cristian Vilar, Benny Thörnberg and Silvia Krug

Department of Electronics Design, Mid Sweden University, Holmgatan, Sundsvall, Sweden

Keywords: Autonomous Wheelchair, Embedded Camera System, Time-of-Flight, Stereo Camera, RANSAC.

Abstract: Autonomously driving Power Wheelchairs (PWCs) are valuable tools to enhance the life quality of their users. In order to enable truly autonomous PWCs, camera systems are essential. Image processing enables the development of applications for both autonomous driving and obstacle avoidance. This paper explores the challenges that arise when selecting a suitable embedded camera system for these applications. Our analysis is based on a comparison of two well-known camera principles, Stereo-Cameras (STCs) and Time-of-Flight (ToF) cameras, using the standard deviation of the ground plane at various lighting conditions as a key quality measure. In addition, we also consider other metrics related to both the image processing task and the embedded system constraints. We believe that this assessment is valuable when choosing between using STC or ToF cameras for PWCs.

# **1 INTRODUCTION**

Power Wheelchairs (PWCs) have improved the quality of life for their users by giving them more independence and transportation facilities. The next step in PWC development is to add features like autonomous driving and obstacle avoidance in order to continue improving the system usability. Caregiver detection and tracking is a step towards the development of a fully autonomous PWC. The caregiver's position can be used as a reference to steer a PWC in a side-byside configuration where the wheelchair follows the caregiver autonomously.

To achieve this, such autonomous driving applications need to collect and store information regarding the PWC's environment using sensors, image cameras, and electronic systems. The required steps include the detection of the surrounding objects, measuring their relative distances and their recognition. These steps have to be executed with high accuracy and precision in order to ensure robust autonomous driving. Camera systems are essential for this, and are already applied to various automotive use cases.

Autonomous driving PWCs and other mobile robots require the ability to detect, measure and recognize objects at relatively short distances in comparison with automotive applications. Visual cameras can detect obstacles but not measure distances with enough accuracy at short ranges. 3D LiDAR cameras, by contrast, can measure long range distances

accurately, but usually do not have a detailed enough resolution to recognize objects (Park et al., 2018). Moreover, these cameras are difficult to embed into the PWC frame due to size and weight limitations. Depth cameras, such as Stereo-Cameras (STCs) or Time-of-Flight (ToF) cameras, are yet another option. They can detect objects, measure distances and provide detailed information about the objects. In addition, they combine depth measurements with visual images to provide additional information useful for object recognition. STCs and ToF cameras are based on different measuring principles and we expect them to have a different performance and impact on the object recognition. In this paper, we intend to investigate these differences with respect to the camera suitability for an autonomously driving PWC.

This investigation is focused on the quality of depth data required for the segmentation of objects above a Ground Plane (GP) at short range distances. The main goal is to evaluate the challenges of STC and ToF camera technologies for autonomous PWC applications and, by extension, for robotics and automated guided vehicles. The paper studies a realworld camera application using depth cameras nonspecifically designed for research that are however available as of the shelf hardware and could meet the embedded system constraints. The scientific contribution of this paper is a qualitative comparison of point cloud data measured by a ToF camera and an STC. To achieve this, we discuss multiple metrics with respect

#### 76

Vilar, C., Thörnberg, B. and Krug, S.

In Proceedings of the 5th International Conference on Vehicle Technology and Intelligent Transport Systems (VEHITS 2019), pages 76-85 ISBN: 978-989-758-374-2

Copyright © 2019 by SCITEPRESS - Science and Technology Publications, Lda. All rights reserved

Evaluation of Embedded Camera Systems for Autonomous Wheelchairs. DOI: 10.5220/0007678700760085

to the constraints introduced by the embedded PWC. Due to the focus on available hardware, our goal is however not to compare the latest algorithms for different subtasks of the depth data processing.

The paper is organized as follows. First, we introduce the fundamentals of depth camera technologies and review other works targeting autonomous PWCs in Section 2. In Section 3, we present the criteria for the camera selection, the camera setup, the required data processing steps as well as the experiment definition. In Section 4, we present and analyze the measurement results. Our results are qualitatively discussed in relation to the experimental goals and the PWC constrains for the selection of a depth camera for autonomous PWC applications in Section 5. Finally, we conclude the paper in Section 6.

# 2 FUNDAMENTALS AND RELATED WORK

## 2.1 Camera Operation Principles

**ToF cameras** measure the time of flight of the reflected light at each point in the image. They use an Infra-Red (IR) active lighting source to illuminate the scene. There are two modes of operation: pulsed lighting or Continuous Wave Modulation (CWM). In pulsed lighting mode, the camera measures the time-of-flight of a very short pulse interval directly. This method has the inherent difficulty of generating and measuring short pulses in order to achieve centime-ter resolution in the range image. CWM means intensity modulated light at a given frequency ( $f_m$ ). It then measures the phase shift ( $\Delta\Phi$ ) between the emitted and reflected light in order to determine the depth ( $d_{ToF}$ ):

$$d_{ToF} = \frac{c}{4\pi f_m} \tag{1}$$

The most common CMW approach is the Lock-in-Pixel architecture (Ringbeck and Hagebeuker, 2007). This approach samples the emitted light in four different phases  $[0^{\circ};90^{\circ};180^{\circ};270^{\circ}]$ . CWM, compared to pulsed operation, reduces the pixel size and thus enables increased image resolution. Typically, the maximum spatial resolution is approximately  $320 \times 240$ pixels and thus significantly lower than for a 2D camera.

The depth resolution depends mainly of technological parameters, in this case, the IR light modulation frequency ( $f_m$ ) (McClure et al., 2010) and errors like wiggling or amplitude related errors (Hussmann et al., 2014). The maximum phase shift limits the depth range ambiguity distance  $(d_{MAX})$ :

$$d_{MAX} = \frac{1}{2(c/f_m)} \tag{2}$$

In addition, ToF sensors suffer from low sensitivity and as a consequence high noise levels (Langmann et al., 2012). Ambient sunlight can interfere with the active illumination, mainly due to the limited dynamic range of the pixels. However, active IR lighting allows nightlight operation and reduces the depth computing costs in comparison with STCs.

In contrast to ToF cameras, **Stereo Cameras** are passive and do not require active illumination under daylight conditions. STCs are based on two single cameras placed side-by-side measuring the depth using principles of triangulation (Gonzalez and Woods, 2010). In STCs, the depth is determined by computing the pixel disparity (D) between both camera images (Kytö et al., 2011) by a block-matching algorithm. Hence, it is a software-based solution and therefore it demands more computing resources and time.

This technology also requires a previous camera calibration in order to compute the pixel disparity properly. Depth  $d_{STC}$  and depth resolution  $\Delta d_{STC}$  are calculated as follows

$$J_{STC} = \frac{fB}{D}$$
 (3)

$$d_{STC} = \frac{d_{STC}^2 \Delta D}{fB} \tag{4}$$

defined by the baseline (distance between cameras) (*B*), focal length (*f*), and precision of disparity computation ( $\Delta D$ ).

The spatial image resolution is limited only by the camera sensor and thus significantly higher than for ToF cameras. An STC is normally not able to operate in nightlight or low-light conditions. It is, however, possible to use active illumination to solve this limitation.

## 2.2 Literature Review

In (Kobayashi et al., 2012), the authors explore the idea of autonomous PWC steering, using the caregiver position as driving reference. This facilitates a reduction of workload for the caregiver and makes a more natural communication between caregiver and the wheelchair user possible. The caregiver is detected and recognized by a rotating LiDAR and an omnidirectional camera placed on a mast. The integration of these bulky system components into a PWC frame is, however, impossible due to the required size. In (Wu et al., 2013), the authors use a ToF kinect camera placed on a mast to detect and track the caregiver walking next to the PWC. Kinect's combination of depth measurements and visual images provides enough information required for caregiver recognition as well as autonomous navigation of a PWC. However, the high camera placement on a mast prevents the detection of obstacles on the ground, which is required for a safe operation of the PWC. Such a mast modifies the ergonomics, structure and appearance of the PWC in a way not suitable for a commercial product.

A better camera placement for ergonomics and safety is the armrest of the PWC. In (Motokucho and Oda, 2014), an STC is placed into the PWC's armrest without disturbing the PWC's manual operation. The lower camera position reduces the scene Field of View (FOV), which decreases the detection probability of complete human shapes. Thus, the position of the caregiver is determined by the recognition of his or her legs.

Another approach is presented in (Udsatid et al., 2012): the caregiver is recognized by measuring the position of the feet above the GP. In this case, the camera is tilted down, looking for objects above the GP. The detected objects are segmented based on a height threshold above the GP. Thresholding-based segmentation is limited by the depth camera resolution at different distances and also by the camera rotation ( $\alpha$ ,  $\beta$ ,  $\gamma$ ) with respect the GP, cf. Figure 2. Due to the movements of the PWC, the camera angles are not constant with respect to the GP. Hence, height-thresholding is not a valid method for GP segmentation in autonomous PWCs and other mobile robotics applications.

In addition to these works targeting the camera system for PWCs, several other studies on robotics and camera technology analyze the ToF and STC performance and calibration methods using flat surfaces or distributed objects as target references, e.g. (Langmann et al., 2012; He et al., 2017; Francis et al., 2015; Kytö et al., 2011; Sun et al., 2018; Kim et al., 2005). Using this methods, a depth camera collects point cloud data at different depths in order to measure accuracy. In our study, we instead use a tilted flat GP as a reference because it is a more representative and realistic experimental setup. The tilted GP allows us to analyze the quality of the measured point cloud data at various distances in a single depth image.

Few other camera comparisons between ToF cameras and STCs exist that compare the technologies e.g. in (Kazmi et al., 2014; Beder et al., 2007). These do however not focus on the dependency on the illumination level, the distance range, the object's reflec-

tivity, and camera power consumption. We consider relevant to analyze the effect of these variables in order to choose a suitable camera in accordance with the application requirements presented in Section 3.1. Therefore, we perform our experiment using different levels of ambient light and different levels of active illumination as well as different object textures. More recent comparisons with a focus on the quality of the depth data are not available to the best of our knowledge.

## **3 METHOD**

## 3.1 **PWC Application Requirements**

Our goal in this paper is to evaluate, which camera technology provides the best performance to enable robust detection of a caregiver. In order to develop such a PWC, a set of constrains regarding the camera specifications and requirements has to be fulfilled, which we will briefly introduce here.

Reliable object detection and recognition is a central requirement of the system. Here, we target the detection of a caregiver by recognizing the caregiver's feet. The following general constraints apply:

- **Operation Environment,** an autonomous PWC has to operate in indoor and outdoor environments and be able to reliably detect the feet of the caregiver under all circumstances.
- **Object Texture,** the camera has to detect objects with different textures and light reflective indexes.
- **Effective Range,** the camera has to measure distances to objects in the range 0–2.5 m from the PWC.
- Minimum Height of a Detectable Objects, the camera has be able to detect small objects above the ground plane in order to detect the feet of the caregiver. Therefore, the GP depth variation should be below 3 cm.
- **Illumination Conditions,** the camera has to be able to operate in both daylight and nightlight conditions. This is required for PWC usability.
- **Real-time Operation,** image capture and depth computation must run in real-time and at a throughput of no less than 10 images per second.
- **Size and Weight,** the camera size and weight are constrained in order to avoid modifying the PWC's dynamic performance. Small camera packages are preferred.

Table 1: Camera specifications.

- **Camera Placement,** the camera has to be fully embedded into the PWC frame in order to improve the overall system safety and ergonomics. The preferred camera placement is the PWC's armrest.
- **Power Consumption,** low power consumption is crucial for the operating range of a battery PWC. Heat dissipation can make the mechanical integration of a camera difficult.

Usually, GP detection and removal is the first processing step for autonomous robot navigation systems (Choi et al., 2014; Zeineldin and El-Fishawy, 2016). Once the GP is removed from the 3D data, it becomes easier to find the objects above it. The minimum size and height of the detectable objects depend mainly on the standard deviation of the GP data. Hence, small objects are more difficult to segment from a noisy GP.

The most used method for GP subtraction on depth images is the Random Sampled Consensus algorithm (RANSAC). It allows fitting planar surfaces from arbitrary 3D point cloud scenes. This method relies on the GP flatness measurement and therefore depends on the camera depth resolution and calibration. We focus on GP data quality in this paper, because of the fundamental link between object segmentation and GP depth variation.

## 3.2 Camera Selection

We have selected a Duo3D MLX (cf. Figure 1a) as the STC and Melexis EVK75123 (cf. Figure 1b) as the ToF camera. The main camera parameters are shown in Table 1.



Figure 1: Selected cameras for experimental evaluation (a) Duo3D MLX (b) Melexis EVK75123.

Both cameras include active illumination and are thus suitable for both daytime and nightlight operation. The cameras can operate in a calibrated point cloud mode and automatically suppress distortions caused by the respective lens. This is important to reduce the calibration and computation effort. The pixel resolution of the two cameras differ, mostly due to the size limitations of the ToF technology.

The pixel disparity for the STC is computed by an auxiliary computer using the application programming interface provided by the camera manufacturer.

Parameter	Camera		
Model	Duo3D MLX	EVK75123	
Technology	STC	ToF CWM	
Frame	$640 \times 480$ pixels	320×240 pixels	
Resolution	040×480 pixels		
Max Frame Rate	98 fps	60 fps	
Pixel Size	$6 \times 6  \mu m$	$15 \times 15  \mu m$	
FOV	170°	110°	
Baseline	30 mm	_	
Light		12 /8 MHz	
Modulation	_	12-40 101112	
Focal Length	2.1 mm	2.8 mm	
IR Lighting	3 A W	0–25 W	
Power	J. <b>+</b> W		
Power	2 W	11 W	
Consumption	2 11	11 W	
ID Wavalangth	850 nm	850 nm	
ik wavelengui	LED	VCSEL	
IR Blocking	no	yes	
Filter	110		
Size	$52 \times 25 \times 13 \text{ mm}$	$80 \times 50 \times 35 \text{ mm}$	

For the ToF, instead, depth computation is perform directly on the camera.

# 3.3 Camera Setup

Both cameras are placed side-by-side on a tripod at the same height (*h*), tilted down 30 degrees ( $\alpha$ ) measuring a flat GP as shown in Figure 2.



Figure 2: Camera setup and camera angle definition.

This camera configuration reproduces a camera placement on the PWC's armrest looking for the caregiver's legs and obstacles above the GP.

# 3.4 Depth Data Processing and Measurement Procedure

We execute a number of pre-processing steps prior to the actual experiments. These initial depth processing steps are shown in Figure 3 and executed separately on data from both cameras.

Camera Range Image
--------------------------

Figure 3: Processing steps for depth data analysis.

First, the range images are transformed into a 3D Point Cloud representation. Example results from this transformation are shown in Figure 4a and Figure 4b. The point cloud data are then rotated using an affine geometrical transformation according to the camera angle ( $\alpha$ ), see Figure 4c. This rotation aligns the measured GP with the camera coordinate system, see Figure 4d. Measured GP data show geometrical distortion and statistical variation due to the camera depth resolution, noise and camera calibration errors. We limited our data analysis into a slide on the X-axis along the Z and Y axes rather that considering all GP data. This allows us to discard the distortion due to the calibration errors and keep only the depth noise into the analysis.



Figure 4: (a) Point cloud data of the ToF camera. (b) Point cloud data of the STC. (c) Original point cloud data representation with respect the ground plane coordinates. (d) Rotation of original point cloud data in order to align it with the Z-Y axes.

ToF raw data is expected to be severely noisy and requires data post-processing (Lenzen et al., 2013). We have used two de-noising methods. Both are implemented directly in the ToF camera. The first is a edge-preserving bilateral filter. It smooths the depth surfaces without distorting the image edges (Tomasi and Manduchi, 1998; Paris et al., 2009). The second method uses an intensity thresholding filter to resolve the unwrapped depth pixels according to their corresponding intensity values (McClure et al., 2010; Cho et al., 2014).

Table 2: Camera parameters used for experiments.

Parameter	Camera			
	STC			
Ambient light	Dark	1201x	2400 lx	*
Gain	1 %	1 %	1 %	_
Exposure (ms)	90	90	40	-
Integration (ms)	-	-	-	0.6
IR Power (W)	3.4	3.4	0	25
Frame Rate (fps)	4	4	4	6

#### **3.5 Performed Experiments**

According to the PWC application requirements defined in Section 3.1, and the camera setup in Section 3.3, we defined the following experiments with the aim to validate both camera technologies:

- Experiment 1 Depth variation
- Experiment 2 Impact of texture
- Experiment 3 Effect of light absorbent materials

In Experiment 1, we measure the statistical variation of GP data under different ambient light conditions using different active illumination intensities and modulation frequencies. Camera parameters and scene conditions are summarized in Table 2. Note that there are experiments at three different levels of ambient light intensities for both cameras. The camera settings for the ToF camera were made independent of the ambient light, whereas the STC needed different settings. Initially, we used a CWM frequency of 20 MHz for the ToF camera and an intensity thresholding filter. To evaluate its impact, we repeated the experiment without applying any filtering on the data prior to analysis. To evaluate the impact of the CWM setting, we performed additional measurements with CWM frequencies of 12, 20, and 32 MHz, respectively. We perform our comparison under static conditions in order to gain a fundamental understanding of the interplay between different parameters first. Due to this, the STC frame rate and ToF integration time have been configured at the same value in all the experiments. The configuration is below the 10 fps we defined for the real-time constraint. However, this is not crucial for the static analysis and future analyses of dynamic cases are planned.

Experiments 2 and 3 analyzed the effect of having non-textured objects and light absorbent materials in the scene. In Experiment 2 we estimated the impact of textured surfaces to the GP measurement while we added reflective and light-absorbent materials into the scene of Experiment 3. These experiments provide us with valuable insights into the GP variation under controlled conditions. In addition, we studied the impact of different camera configurations and operating principles on the quality of the ground plane data and thus the possibility of GP removal from the scene for later object recognition. This is essential in order to select and implement a corresponding camera system into a PWC at a later point in time.

# 4 RESULTS AND ANALYSIS

## 4.1 Depth Variation Measurements

In Experiment 1, we analyzed the GP depth variation by computing the standard deviation ( $\sigma$ ) of the measured height along the GP Y-axis as is shown in Figure 2 at different ambient illumination conditions. We believe this is a good metric to determine the minimum detectable height of objects located above the GP with respect to the measured distance. Results for the STC are shown in Figure 5, and for the ToF camera in Figure 6.



Figure 5: STC GP measurement of the Y-axis (height) and  $\sigma$  along the Z-axis (depth) under different ambient light conditions.

The upper graphs in Figures 5 to 9 show point cloud data after rotation with  $\alpha$ , as illustrated in Figure 4. Ideally, we should see a thin, straight line, perfectly aligned with the horizontal axis at zero level. However, real-world measurements show limitations from e.g. camera calibration and noise.

The results from the ToF camera shown in Figure 6 are invariant to the ambient light intensity. By contrast, the STC results greatly depend on the ambient light intensity. In dark conditions, when only STC active illumination is used, the measurement is



Figure 6: ToF GP measurement of the Y-axis (height) and  $\sigma$  along the Z-axis (depth) under different ambient light conditions with intensity thresholding filter.

very noisy, even at short distances. When the ambient light intensity increases, the GP depth variation is reduced and the maximum measurement range increases accordingly.

The same analysis was performed without intensity thresholding filter for the ToF camera. Figure 7 shows the results. In this case, pixels with low intensi-



Figure 7: ToF GP measurement of the Y-axis (height) and  $\sigma$  along the Z-axis (depth) under different ambient light conditions without intensity thresholding filter.

ties are not removed and thus cause a depth measurement error. Figures 6 and 7 both show that the distance of the ToF measurements is limited. Although the used modulation frequency of 20MHz provides a  $d_{MAX}$  of 7.5 m according to Equation 2, the practical measurement range is shorter in both cases. When using the intensity thresholding filter it becomes even less than 2 m, see Figure 6. The reason for this shorter distance is the limited intensity of the reflected light. The filter removes depth pixels whose intensity values are lower than a specified threshold. This threshold is based on low intensity levels being an indication of low confidence in the phase measurements. Thus, pixels above approximately 2.5 m do not have enough intensity levels and are therefore deleted.

Finally, we assessed the impact of different CWM frequencies of the ToF camera. As shown in Figure 8, the maximum range and the GP depth variation are reduced with an increasing CWM frequency.



Figure 8: ToF GP measurement using different different CWM frequencies.

The  $\sigma$  of the ToF depth data increases for greater distances in both camera measurements, but is more severe for the STC. This result was expected due to the STC depth resolution definition according to Equation 4, which decreases quadratically with distance  $d_{STC}$ . Thus, the non-linear behavior of  $\Delta d_{STC}$  in practice limits the maximum distance  $d_{STC}$  in which objects can be detected above the GP.

The standard deviation of the ToF depth data is increasing linearly according to the distance (cf. Figure 6. This linear behavior matches that of other ToF cameras analyzed in (Shi et al., 2011). The maximum range is mainly limited by the unwrapped depth pixels, caused by non-detectable phase shifts greater than 360 degrees. If they are not removed by e.g. an intensity thresholding filter, then the GP variation will increase (cf. Figure 7). Standard deviation measurements for both cameras are summarized in Table 3.

## 4.2 Impact of Texture

In Experiment 2, we measured a GP with and without a textured pattern in order to test the lack of a texture in the STC's block-matching algorithm. The results are shown in Figure 9.

To perform the experiment, a non-textured flat white surface with a length of 2.5 m was placed di-

GPZ[m]		σ [mm]			
	STC	ToF			
		12 MHz	20 MHz	32 MHz	
0.5	12.7	13.3	12.3	8	
1	10.5	17.1	19.8	6.4	
1.5	20.3	25.6	19.6	27.2	
2	31.5	32.7	16.4	_	
2.5	75.6	41.7	-	-	
3	84.1	56.4	_	_	



Figure 9: STC GP measurement with textured and non-textured GP surface.

rectly on top of the GP at a distance of 0.5 to 3 m from the camera, along the GP. Both results are measured in the same ambient light intensity, active IR illumination, and camera configuration.

The measurements of a non-textured GP show the effect of an erroneous result from the disparity computation due to difficulties matching  $8 \times 8$  pixel blocks without unique texture. As a result, the non-textured GP becomes noisy, making it difficult to detect small objects.

#### 4.3 Effect of Light Absorbent Materials

In Experiment 3, we measured the effect of adding light absorbent and light reflective patches on the GP surface. The patches are 25 cm long and placed at a distance of 0.6–0.85 m from the camera, along the GP. Qualitative results for the STC are shown in Figure 10, and for the ToF camera in Figure 11.

The light absorbing material has no major impact on the depth measurements of the GP by the STC. It is important to note that for both cases  $\sigma_{STC}$  of the depth data increases due to the patch edges and not



Figure 10: STC GP measurement with light absorbent and light reflective material patches.

because of the light absorbing material itself. When a highly reflective material patch is used, the GP level changes significantly and causes a depth inaccuracy in the measurement.

The effect of the IR light reflection for the ToF has been measured in Figure 11. Here, the camera operates at a CWM frequency of 32 MHz. Both patches are placed in each scene corresponding to a sub-figure. The light absorbing patch is shown as the dark rectangular shape at the bottom of each sub-figure, while the light reflector is shown above it (e.g. the bright blue rectangular shape in Figure 11d).



Figure 11: ToF range image data at different relative active illumination powers: (a) 100%, (b) 50%, (c) 25%, (d) 10%.

At 100 % power, the light absorbing patch reduces the intensity of the reflected light and the patch becomes difficult to detect. When the active illumination power is decreased, the absorbing patch becomes undetectable, while the reflective patch is still perfectly detectable, even at low illumination powers.

## 5 DISCUSSION

Our measurements show that in general  $\sigma$  increases with the distance and that a maximum distance of around 2.5 m can be achieved with both cameras. Both cameras chosen for our study show similar  $\sigma$  of the GP under daylight conditions and up to a distance of two meters. The  $\sigma$  of roughly 3 cm means that objects higher than 3 cm can be detected above the GP with a confidence of 68 %. As such, both fulfill the general requirements of target effective range, and the minimum height of a detectable object as defined in Section 3.1. However, we expect objects closer to the cameras to be more accurately detected due to a lower  $\sigma$  of the GP for these measurements.

For the STC, the parameters  $\Delta d_{STC}$ ,  $d_{STC}$  and  $\sigma_{STC}$  are improved when the STC is working in optimal ambient light conditions. We believe that this effect is caused by an improved signal-to-noise-ratio (SNR) at stronger illumination levels. Lower SNR degrades the performance of the block-matching disparity algorithm and thus  $\Delta D$  increases as reported by (Sabater et al., 2011). In addition, dark illumination levels require higher exposure times, limiting then the maximum frame rate. In a PWC application, this effect has to be considered when ensuring real-time operation and dynamic movement. In practise, camera images can be blurred if objects in the scene or the PWC are moving. Especially, lower illumination conditions are expected to be critical due to the higher exposure time. Blurring will, as a consequence, degrade the block-matching algorithm performance.

For the ToF cameras, the maximum range depends mainly on the CWM frequency (Hussmann et al., 2014; Dashpute et al., 2018). It decreases with higher modulation frequencies. In practical applications, increasing the CWM frequency triggers phase shift errors, causing higher depth variation towards the end of the observed range. This problem can be solved by limiting the scene objects within an experimentally obtained maximum distance.

Even if all the scene objects are inside this safe distance range, we can detect unwrapped depth pixels as shown in Figure 7 for the ToF camera. These pixels can be removed by an intensity thresholding filter, but the useful distance range will be further reduced as a consequence. This problem can be mitigated partially by increasing the active illumination power. However, using active illumination requires a higher power consumption that cannot be avoided if an extended distance range is required. This is especially crucial as the ToF camera range was already shorter compared to the STC and lower than the limit defined in Section 3.1. As for STC, ToF dynamic performance can also be limited due to moving objects in the scene under low active illumination conditions. Moving objects can require to reduce the integration time in that case, but and as a consequence, the noise level and  $\sigma$  will increase (Gay-Bellile et al., 2015), limiting thus the maximum distance range.

The presence of light absorbent materials poses a severe challenge for the ToF camera. Light absorbent objects cannot be detected by this type of camera, even at relatively short distances. This dependency on the material's reflectivity makes caregiver detection a challenge when low reflective clothing are used. As a countermeasure the active illumination power can be increased at the cost of higher power consumption.

By contrast, STCs can detect light absorbent objects under ambient daylight conditions. However, reflective objects cause inaccurate depth measurements by the STCs. This inaccuracy is most likely caused by the lack of texture on the saturated reflective patch. A similar behavior was observed for the non-textured GP. Disparity computation errors occur due to the lack of texture. If such errors originate from saturated regions, the problem could probably be mitigated if a high dynamic range imager were used. Where the levels of GP texture are limited, increasing the size of the pixel block used to compute pixel disparities could help. We can expect this problem for indoor scenarios, icy/wet conditions outdoors, or for clothing with low levels of texture. However, GPs in outdoor conditions normally provide good enough texture for STCs.

Since STCs are able to operate in daylight conditions without additional active illumination, a lot of heat dissipation and power consumption can be avoided. However, ToF cameras require active illumination in all scenarios in order to maintain a high level of SNR. As a consequence, ToF cameras have much higher levels of heat dissipation that require a careful thermal design. Embedding electronics into the armrest of a PWC can be a challenge at higher levels of heat dissipation. This is never the case when STCs are used in daylight conditions.

# 6 CONCLUSIONS

In this paper, we reviewed challenges related to integration and the use of depth cameras on PWCs.

The main limitation of ToF cameras is the noise level in combination with the active illumination power. STCs, for their part, are limited by the level of ambient illumination and by the texture of the objects in order to successfully compute the pixel disparities.

Both STC and ToF camera technologies are suit-

able for e.g. obstacle or caregiver detection by the PWC but we prefer STC because of the lower heat dissipation and power savings in daylight conditions, as well as the more robust detection of light absorbent materials. The results from this study should be relevant for any low-speed vehicle or autonomous robot.

As a future step, we plan to assess the dynamic performance of both cameras under dynamic conditions with moving objects in the scene. We believe that the dynamic performances will be degraded under low illumination levels and higher exposure or integration times.

## REFERENCES

- Beder, C., Bartczak, B., and Koch, R. (2007). A Comparison of PMD-Cameras and Stereo-Vision for the Task of Surface Reconstruction using Patchlets. In *Conference on Computer Vision and Pattern Recognition* (CVPR), pages 1–8.
- Cho, J., Choi, J., Kim, S.-J., Park, S., Shin, J., Kim, J. D., and Yoon, E. (2014). A 3-D Camera With Adaptable Background Light Suppression Using Pixel-Binning and Super-Resolution. *IEEE Journal of Solid-State Circuits*, 49(10):2319–2332.
- Choi, S., Park, J., Byun, J., and Yu, W. (2014). Robust Ground Plane Detection from 3D Point Clouds. In 14th International Conference on Control, Automation and Systems (ICCAS), pages 1076–1081.
- Dashpute, A., Anand, C., and Sarkar, M. (2018). Depth Resolution Enhancement in Time-of-Flight Cameras Using Polarization State of the Reflected Light. *IEEE Transactions on Instrumentation and Measurement*, PP(1):1–9.
- Francis, S. L. X., Anavatti, S. G., Garratt, M., and Shim, H. (2015). A ToF-Camera as a 3D Vision Sensor for Autonomous Mobile Robotics. *International Journal* of Advanced Robotic Systems, 12(11):156.
- Gay-Bellile, V., Bartoli, A., Hamrouni, K., Sayd, P., Bourgeois, S., and Belhedi, A. (2015). Noise modelling in time-of-flight sensors with application to depth noise removal and uncertainty estimation in threedimensional measurement. *IET Computer Vision*, 9(6):967–977.
- Gonzalez, R. and Woods, R. (2010). *Digital Image Processing (Third Edition)*. Prentice-Hall Inc.
- He, Y., Liang, B., Zou, Y., He, J., and Yang, J. (2017). Depth Errors Analysis and Correction for Time-of-Flight (ToF) Cameras. *Sensors*, 17(1):92.
- Hussmann, S., Knoll, F., and Edeler, T. (2014). Modulation method including noise model for minimizing the wiggling error of tof cameras. *IEEE Transactions on Instrumentation and Measurement*, 63(5):1127–1136.
- Kazmi, W., Foix, S., Alenyà, G., and Andersen, H. J. (2014). Indoor and outdoor depth imaging of leaves with time-of-flight and stereo vision sensors: Analy-

sis and comparison. *ISPRS Journal of Photogramme*try and Remote Sensing, 88:128–146.

- Kim, W. S., Ansar, A. I., Steele, R. D., and Steinke, R. C. (2005). Performance Analysis and Validation of a Stereo Vision System. In *International Conference on Systems, Man and Cybernetics*, pages 1409–1416.
- Kobayashi, Y., Suzuki, R., and Kuno, Y. (2012). Robotic Wheelchair with Omni-directional Vision for Moving alongside a Caregiver. In 38th Annual Conference on IEEE Industrial Electronics Society (IECON), pages 4177–4182.
- Kytö, M., Nuutinen, M., and Oittinen, P. (2011). Method for measuring stereo camera depth accuracy based on stereoscopic vision. In *Three-Dimensional Imaging*, *Interaction, and Measurement*.
- Langmann, B., Hartmann, K., and Loffeld, O. (2012). Depth Camera Technology Comparison and Performance Evaluation. In 1st International Conference on Pattern Recognition Applications and Methods (ICPRAM), pages 438–444.
- Lenzen, F., Kim, K. I., Schäfer, H., Nair, R., Meister, S., Becker, F., Garbe, C. S., and Theobalt, C. (2013). Denoising strategies for time-of-flight data. In *Time-of-Flight and Depth Imaging. Sensors, Algorithms, and Applications*, pages 25–45. Springer.
- McClure, S. H., Cree, M. J., Dorrington, A. A., and Payne, A. D. (2010). Resolving depth-measurement ambiguity with commercially available range imaging cameras. In *Image Processing: Machine Vision Applications III.*
- Motokucho, T. and Oda, N. (2014). Vision-based Human-Following Control using Optical Flow Field for Power Assisted Wheelchair. In 13th International Workshop on Advanced Motion Control (AMC), pages 266–271.
- Paris, S., Kornprobst, P., Tumblin, J., Durand, F., et al. (2009). Bilateral Filtering: Theory and Applications. *Foundations and Trends* (R) in Computer Graphics and Vision, 4(1):1–73.
- Park, K., Kim, S., and Sohn, K. (2018). High-Precision Depth Estimation with the 3D LiDAR and Stereo Fusion. In *International Conference on Robotics and Automation (ICRA)*, pages 2156–2163.
- Ringbeck, T. and Hagebeuker, B. (2007). A 3D time of flight camera for object detection. In Optical 3-D Measurement Techniques.
- Sabater, N., Morel, J.-M., and Almansa, A. (2011). How accurate can block matches be in stereo vision? SIAM Journal on Imaging Sciences, 4(1):472–500.
- Shi, B.-Q., Liang, J., and Liu, Q. (2011). Adaptive simplification of point cloud using k-means clustering. *Computer-Aided Design*, 43(8):910–922.
- Sun, P., Lu, N. G., Dong, M. L., Yan, B. X., and Wang, J. (2018). Simultaneous All-Parameters Calibration and Assessment of a Stereo Camera Pair Using a Scale Bar. Sensors (Basel, Switzerland), 18(11):1–19.
- Tomasi, C. and Manduchi, R. (1998). Bilateral Filtering for Gray and Color Images. In 6th International Conference on Computer Vision, pages 839–846.
- Udsatid, P., Niparnan, N., and Sudsang, A. (2012). Human Position Tracking for Side By Side Walking Mo-

bile Robot using Foot Positions. In International Conference on Robotics and Biomimetics (ROBIO), pages 1374–1378.

- Wu, B.-F., Jen, C.-L., Li, W.-F., Tsou, T.-Y., Tseng, P.-Y., and Hsiao, K.-T. (2013). RGB-D Sensor Based SLAM and Human Tracking with Bayesian Framework for Wheelchair Robots. In *International Conference on Advanced Robotics and Intelligent Systems* (ARIS), pages 110–115.
- Zeineldin, R. A. and El-Fishawy, N. A. (2016). Fast and Accurate Ground Plane Detection for the Visually Impaired from 3D Organized Point Clouds. In SAI Computing Conference, pages 373–379.